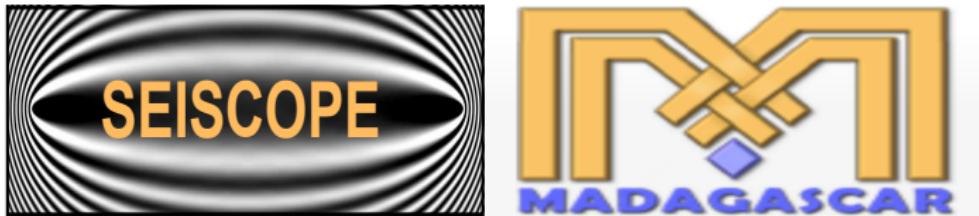


An Introduction to Modeling, Imaging and Full Waveform Inversion

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- 1 The wave equation
- 2 Forward modeling
- 3 Absorbing boundary condition
- 4 Seismic imaging/migration
- 5 Full waveform inversion (FWI)

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Particle velocity vector $\mathbf{v} = [v_x, v_y, v_z]^T$; stress vector $\boldsymbol{\sigma} = [\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{yz}, \sigma_{xz}, \sigma_{xy}]^T$

- Newton's law: $\rho \partial_t v_i = \partial_j \sigma_{ij}, \quad i, j \in \{x, y, z\} = \{1, 2, 3\}$
- Generalized Hooke's law: $\sigma_{ij} = c_{ijkl} \epsilon_{kl}$

Voigt indexing: (11) \rightarrow 1, (22) \rightarrow 2, (33) \rightarrow 3, (23) = (32) \rightarrow 4, (13) = (31) \rightarrow 5, (12) = (21) \rightarrow 6

$$\begin{cases} \rho \partial_t \mathbf{v} = D \boldsymbol{\sigma} + \mathbf{f}_v \\ \partial_t \boldsymbol{\sigma} = C D^T \mathbf{v} + \mathbf{f}_{\sigma} \end{cases}, \quad C = \begin{bmatrix} c_{11} & c_{12} & c_{13} & c_{14} & c_{15} & c_{16} \\ \cdot & c_{22} & c_{23} & c_{24} & c_{25} & c_{26} \\ \cdot & \cdot & c_{33} & c_{34} & c_{35} & c_{36} \\ \cdot & \cdot & \cdot & c_{44} & c_{45} & c_{46} \\ \cdot & \text{SYM} & \cdot & \cdot & c_{55} & c_{56} \\ \cdot & \cdot & \cdot & \cdot & \cdot & c_{66} \end{bmatrix}, \quad D^T = \begin{bmatrix} \partial_x & 0 & 0 \\ 0 & \partial_y & 0 \\ 0 & 0 & \partial_z \\ 0 & \partial_z & \partial_y \\ \partial_z & 0 & \partial_x \\ \partial_y & \partial_x & 0 \end{bmatrix} \quad (1)$$

- Triclinic: 21 independent coefficients in C
- Monoclinic: 13 independent coefficients in C
- Orthorombic: 9 independent coefficients in C
- Transverse isotropic: 5 independent coefficients in C

Isotropic elastic medium:

$$C = \begin{bmatrix} \lambda + 2\mu & \mu & \mu & 0 & 0 & 0 \\ \mu & \lambda + 2\mu & \mu & 0 & 0 & 0 \\ \mu & \mu & \lambda + 2\mu & 0 & 0 & 0 \\ 0 & 0 & 0 & \mu & 0 & 0 \\ 0 & 0 & 0 & 0 & \mu & 0 \\ 0 & 0 & 0 & 0 & 0 & \mu \end{bmatrix} \quad (2)$$

Acoustic medium ($\mu = 0$): pressure $p = (\sigma_{xx} + \sigma_{yy} + \sigma_{zz})/3$

$$\begin{cases} \rho \partial_t \mathbf{v} = \nabla p \\ \partial_t p = \kappa \nabla \cdot \mathbf{v}, \kappa = \rho c^2 \end{cases} \quad (3)$$

1st order equation system \rightarrow 2nd order equation

$$\frac{1}{c^2} \partial_{tt} p - \rho \nabla \cdot \left(\frac{1}{\rho} \nabla p \right) = f \quad (4)$$

Constant density:

$$\left(\frac{1}{c^2} \partial_{tt} - \nabla^2 \right) p = f, \nabla^2 = \partial_{xx} + \partial_{yy} + \partial_{zz} \quad (5)$$

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Modeling=Simulate wave propagation by solving **wave equation numerically**

Which numerical method?

- ① Finite difference method (FDM)
- ② Finite element method (FEM) → Spectral element method (SEM)
- ③ Fourier/spectral method: pseudo spectral method (PSM), lowrank finite difference

Tradeoff between computation and accuracy?

- FDM outperforms FEM and PSM due to excellent efficiency;
- SEM, PSM, lowrank FD arrive at spectral accuracy in space;
- FEM, SEM are more flexible to handle complex topography, generally more expensive than FDM;

In which domain: **Time domain** or Frequency domain?

1. Finite difference method (FDM) in time domain

- direct discretization of the original differential equation, both in time and in space
- explicit time integration:** $n \rightarrow n + 1$, $(\frac{1}{c^2} \partial_{tt} - \partial_{xx})p = f$

$$\frac{p_j^{n+1} - 2p_j^n + p_j^{n-1}}{\Delta t^2 c^2} - \partial_{xx} p^n = f^n \Rightarrow p_j^{n+1} = 2p_j^n - p_j^{n-1} + \frac{\Delta t^2 c^2}{\Delta x^2} (p_{j+1}^n - 2p_j^n + p_{j-1}^n) \quad (6)$$

- implicit time integration:** $n \rightarrow n + 1$, matrix inversion

$$\frac{p^{n+1} - 2p^n + p^{n-1}}{\Delta t^2 c^2} - \partial_{xx} p^{n+1} = f^n \quad (7)$$

$$\Rightarrow A p^{n+1} = b, A = \begin{bmatrix} 2 + \alpha_2 & -1 & & & \\ -1 & \ddots & \ddots & & \\ & \ddots & \ddots & \ddots & \\ & & \ddots & \ddots & -1 \\ & & & -1 & 2 + \alpha_M \end{bmatrix}, \alpha_j = \frac{\Delta x^2}{c_j^2 \Delta t^2} \quad (8)$$

- Finite difference method (FDM) in frequency domain: solve Helmholtz equation

 - direct discretization of the original differential equation, both in frequency and space
 - implicit scheme with matrix inversion $\tilde{\mathbf{p}} = \mathbf{A}^{-1}\tilde{\mathbf{f}}$

$$\left(\frac{1}{c^2}\partial_{tt} - \partial_{xx}\right)\mathbf{p} = \mathbf{f} \Rightarrow -\frac{\omega^2}{c^2}\tilde{\mathbf{p}} - \partial_{xx}\tilde{\mathbf{p}} = \tilde{\mathbf{f}} \Rightarrow -\frac{\omega^2}{c_j^2}\tilde{p}_j - \frac{\tilde{p}_{j+1} - 2\tilde{p}_j + \tilde{p}_{j-1}}{\Delta x^2} = \tilde{f} \quad (9)$$

$$\Rightarrow \underbrace{\begin{bmatrix} \ddots & & \ddots & & \\ & \ddots & & & \\ & & -\frac{1}{\Delta x^2} & \frac{2}{\Delta x^2} - \frac{\omega^2}{c_j^2} & -\frac{1}{\Delta x^2} & \cdots \\ & & & \ddots & & \ddots \end{bmatrix}}_A \underbrace{\begin{bmatrix} \vdots \\ p^{n-1} \\ p^n \\ p^{n+1} \\ \vdots \end{bmatrix}}_{\tilde{\mathbf{p}}} = \underbrace{\begin{bmatrix} \vdots \\ \tilde{f} \\ \vdots \end{bmatrix}}_{\tilde{\mathbf{f}}} \quad (10)$$

- very efficient for multiple sources due to only 1 time of matrix inversion:
 $[\tilde{\mathbf{p}}_1, \tilde{\mathbf{p}}_2, \dots] = \mathbf{A}^{-1}[\tilde{\mathbf{f}}_1, \tilde{\mathbf{f}}_2, \dots]$
- easy to incorporate attenuation $\tilde{c}(\omega) = c_0(1 - \frac{i\text{sign}(\omega)}{2Q}) \rightarrow$ more diagonal dominant for stable matrix inversion
- filling the matrix in multifrontal parallel solver: MUMPS, umfpack, ...

2. Finite element method (FEM): matrix inversion at each time step

\Rightarrow solving the weak form of the differential equation, test/basis function $\phi_j \in [0, 1]$

Second order wave equation with displacement

$$\int_0^1 \left(\partial_{tt} u(x, t) - c^2(x) \partial_{xx} u(x, t) - f(x, t) \right) \phi_j(x) dx = 0 \quad (11)$$

\Rightarrow state variable $u(x, t) = \sum_{i=1}^N u_i(t) \phi_i(x)$: polynomial expansion separable over space and time

$$\sum_i \partial_{tt} u_i \underbrace{\int_0^1 \phi_i \phi_j dx}_{M_{ji}} + c^2 \sum_i u_i \underbrace{\int_0^1 \partial_x \phi_i \partial_x \phi_j dx}_{K_{ji}} = \int_0^1 f \phi_j dx \Rightarrow M \partial_{tt} \mathbf{u} + K \mathbf{u} = \mathbf{f}' \quad (12)$$

$$M \frac{\mathbf{u}^{n+1} - 2\mathbf{u}^n + \mathbf{u}^{n-1}}{\Delta t^2} + Ku^n = \mathbf{f}' \Rightarrow \mathbf{u}^{n+1} = 2\mathbf{u}^n - \mathbf{u}^{n-1} + M^{-1}(\mathbf{f}' - Ku^n) \quad (13)$$

- SEM (Komatsisch et al., 1998): specific mesh, diagonal mass matrix M^{-1} for efficient wave extrapolation by choosing GLL collocation points

3. Fourier/spectral methods: computing spatial derivative using Fourier transform

- Pseudo spectral method (PSM):

$$f(x) = \int f(k) e^{ikx} dk, \Rightarrow \partial_x f = \int ikf(k) e^{ikx} dk, \partial_{xx} f = \int -k^2 f(k) e^{ikx} dk \quad (14)$$

$$\frac{1}{c^2} \partial_{tt} p = (\partial_{xx} + \partial_{zz}) p \Rightarrow p^{n+1} = 2p^n - p^{n-1} + \Delta t^2 c^2 F^{-1} [-(k_x^2 + k_z^2) F p^n] \quad (15)$$

- Lowrank finite difference method (Fomel et al., 2013):

$$p(\mathbf{x}, t + \Delta t) = \int p(\mathbf{k}, t) e^{i\phi(\mathbf{x}, \mathbf{k}, \Delta t)} d\mathbf{k}, = \int e^{i\mathbf{k} \cdot \mathbf{x}} W(\mathbf{x}, \mathbf{k}) p(\mathbf{k}, t) d\mathbf{k}, \quad (16)$$

$$W(\mathbf{x}, \mathbf{k}) = e^{i[\phi(\mathbf{x}, \mathbf{k}, \Delta t) - \mathbf{k} \cdot \mathbf{x}]}, W(\mathbf{x}, \mathbf{k}) \approx \sum_{m=1}^M \sum_{n=1}^N W(\mathbf{x}_n, \mathbf{k}_m) a_{mn} W(\mathbf{x}_n, \mathbf{k}) \quad (17)$$

Approximate lowrank decomposition leads to

$$p(\mathbf{x}, t + \Delta t) \approx \sum_{m=1}^M W(\mathbf{x}, \mathbf{k}_m) \sum_{n=1}^N a_{mn} \int e^{i\mathbf{k} \cdot \mathbf{x}} W(\mathbf{x}_n, \mathbf{k}) p(\mathbf{k}, t) d\mathbf{k}, \quad (18)$$

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PA (Paraxial approximation, radiation) boundary condition (Clayton and Engquist, 1977):
 → cancel the reflection on the boundary using waves propagating in opposite direction according to pseudo differential operator decomposition

$$\left(\frac{1}{c^2}\partial_{tt} - \partial_{xx} - \partial_{zz}\right)p = -\left(\partial_x + \frac{1}{c}\partial_t\sqrt{1-S^2}\right)\left(\partial_x - \frac{1}{c}\partial_t\sqrt{1-S^2}\right)p = 0, S = \frac{\partial_z}{\partial_t/c} \quad (19)$$

- 1st order approximation: $\sqrt{1-S^2} \approx 1$, perfect in 1D $S = 0$, accurate within a specific range of angles in multi-dimensions!

$$\left(\frac{1}{c^2}\partial_{tt} - \partial_{xx}\right)p = \left(\frac{1}{c}\partial_t - \partial_x\right)\left(\frac{1}{c}\partial_t + \partial_x\right)p = 0 \Rightarrow x \in [0, L] \begin{cases} \frac{1}{c}\partial_t p(0, t) - \partial_x p(0, t) = 0 \\ \frac{1}{c}\partial_t p(L, t) + \partial_x p(L, t) = 0 \end{cases} \quad (20)$$

- 2nd order approximation: $\sqrt{1-S^2} \approx 1 - \frac{1}{2}S^2$

$$\left(\partial_x - \frac{\partial_t}{c} + \frac{c\partial_{zz}}{2\partial_t}\right)p = 0 \Rightarrow \partial_{xt}p - \frac{1}{c}\partial_{tt}p + \frac{c}{2}\partial_{zz}p = 0(x=0) \quad (21)$$

Sponge layers/Gaussian taper boundary condition (Cerjan et al., 1985):

→ multiply an exponential decaying factor $e^{-d_x \Delta t}$ in boundary layers at each time step

- easy to implement, **stable** in any anisotropic medium!
- a good choice for the damping profile to achieve PML-like effect:

$$d_x = -\frac{3v_{\max}}{2L} \log(R_c) \left(\frac{x}{L}\right)^2, R_c = 10^{-3} \sim 10^{-6} \quad (22)$$

PML(Perfectly matched layer)(Bérenger, 1994): 1st order wave equation system

→ coordinate transformation in complex-valued anisotropic medium

$$\tilde{x} = x + \frac{1}{i\omega} \int_0^x d_x(s) ds \Rightarrow \partial_{\tilde{x}} = \frac{1}{1 + \frac{d_x}{i\omega}} \partial_x, \quad (23)$$

- intrinsically **unstable** in anisotropic medium for long duration simulation!
- Frequency domain multiplication → Time domain convolution, implemented by recursion with memory variables

$$\begin{cases} \partial_t \mathbf{v} = \frac{1}{\rho} \nabla p \\ \partial_t p = \kappa \nabla \cdot \mathbf{v} \end{cases} \Rightarrow \begin{cases} \partial_t v_i = \frac{1}{\rho} \partial_i p - d_i v_i, i \in \{x, y, z\} \\ \partial_t p = \kappa (\partial_x v_x + \partial_y v_y + \partial_z v_z) - (d_x + d_y + d_z) p \end{cases} \quad (24)$$

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- Deconvolution (U/D) IC (Claerbout, 1971): Recorded signal (upcoming wavefield at receivers) = Earth's reflectivity * downgoing source wavelet (downgoing wavefield).

$$U(\mathbf{x}, t) = R(\mathbf{x}) * D(\mathbf{x}, t) \Rightarrow R(\mathbf{x}) = \frac{U(\mathbf{x}, t)}{D(\mathbf{x}, t)}, \text{unstable} \quad (25)$$

- Zero-lag crosscorrelation IC → illumination compensation

$$\begin{aligned} I(\mathbf{x}) &= \sum_{i=1}^{nt} U(\mathbf{x}, t_i) D(\mathbf{x}, t_i) \Rightarrow \\ I'(\mathbf{x}) &= \frac{\sum_{i=1}^{nt} U(\mathbf{x}, t_i) D(\mathbf{x}, t_i)}{\sum_{i=1}^{nt} D^2(\mathbf{x}, t_i)} = \frac{U_1 D_1 + \dots + U_{i\max} D_{i\max} + \dots + U_{nt} D_{nt}}{D_1 D_1 + \dots + D_{i\max} D_{i\max} + \dots + D_{nt} D_{nt}} \end{aligned} \quad (26)$$

requires simultaneous accessing to the source and receiver wavefields

- Excitation amplitude IC (Chang and McMechan, 1986): taking maximum absolute of downgoing wavefield at excitation time t_i

$$I(\mathbf{x}) = \frac{U(\mathbf{x}, t_i)}{\max |D(\mathbf{x}, t_i)|} \quad (27)$$

knowing t_i is enough, no need for storing or reconstructing source wavefield

Extended IC (Sava and Fomel, 2006): redundant dimensions to evaluate energy focusing

- Conventional IC: $I(\mathbf{x}) = R(\mathbf{x}, t = 0)$, $R(\mathbf{x}, t) = U(\mathbf{x}, t) * D(\mathbf{x}, t)$
- Space-shift** IC: $\mathbf{h} = 0 \rightarrow$ conventional IC

$$I(\mathbf{x}, \mathbf{h}) = R(\mathbf{x}, \mathbf{h}, t = 0), R(\mathbf{x}, \mathbf{h}, t) = U(\mathbf{x} + \mathbf{h}, t) * D(\mathbf{x} - \mathbf{h}, t) \quad (28)$$

- Time-shift** IC: $\tau = 0 \rightarrow$ conventional IC

$$I(\mathbf{x}, \tau) = R(\mathbf{x}, \tau, t = 0), R(\mathbf{x}, \tau, t) = U(\mathbf{x}, t + \tau) * D(\mathbf{x}, t - \tau) \quad (29)$$

- Practical usage in RTM and FWI: horizontal subsurface offset shift, $(x \pm h, y, z)$
- Implemented in frequency domain via Fourier transform

$$R(\mathbf{m}, \mathbf{h}) = \sum_{\omega} U(\mathbf{x} + \mathbf{h}, \omega) D^*(\mathbf{x} - \mathbf{h}, \omega) \quad R(\mathbf{m}, \tau) = \sum_{\omega} U(\mathbf{x}, \omega) D^*(\mathbf{x}, \omega) e^{2i\omega\tau} \quad (30)$$

- Excitation amplitude IC+ extended time/space shift \Rightarrow an easier way to obtain **angle gathers** with low computation and memory cost? $R(\mathbf{x}, \tau) \Rightarrow R(\mathbf{x}, \theta)$

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Objective=Waveform misfit

$$\min_m C(m) = \frac{1}{2} \|d_{cal}(m) - d_{obs}\| \quad (31)$$

Given an **initial model m_0** , iteratively update the model

$$m^{k+1} = m^k + \gamma_k \Delta m^k \quad (32)$$

using different optimization methods: $\Delta m^k = -H^{-1} \nabla_m C$

- Steepest descent method (SDM): $\Delta m^k = -\nabla_m C$
- Nonlinear conjugate gradient (NLCG) (Pica et al., 1990):

$$\Delta m^k = d_k = -\nabla_m C + \beta d_{k-1}$$
- Quasi-Newton method, L-BFGS (Brossier, 2011): $H \approx H_a$ approximate Hessian using previously memorized gradients $\nabla C|^k, \nabla C|^{k-1}, \nabla C|^{k-2}, \dots$
- Newton method, Truncated Newton (Santosa and Symes, 1988; Métivier et al., 2014): compute Hessian vector product using CG method within few iterations
- Gauss-Newton (Shin et al., 2001): $H_a = J^\dagger J$, approximate Hessian using first order scattering information

Frequency/Fourier domain FWI (Pratt et al., 1998): $-(\frac{1}{v^2}\omega^2 + \nabla^2)\tilde{p} = \tilde{f}$

$$C(m) = \frac{1}{2} \sum_s \sum_r \sum_{\omega} |d_{cal}^{s,r}(m, \omega) - d_{obs}^{s,r}(\omega)|^2, d_{cal}^{s,r}(m, \omega) = R_{s,r} \tilde{p} \quad (33)$$

- Multiscale approach: from low frequency to high frequency
- Extremely efficient for multisource problem: same A^{-1} for any source \tilde{f}_i , $[\tilde{p}_1, \tilde{p}_2, \dots] = A^{-1}[\tilde{f}_1, \tilde{f}_2, \dots]$
- Easy for incorporating seismic attenuation: complex-valued velocity
- Super-big matrix inversion requiring large storage in 3-D
- No way for data windowing and selective inversion
- → Laplacian-Fourier domain (Shin and Cha, 2009): Fourier domain with damped traces

Time domain: Convenient for data pre-processing: windowing, filtering, denoising

$$C(m) = \frac{1}{2} \sum_s \sum_r \int_0^T dt |d_{cal}^{s,r}(m, t) - d_{obs}^{s,r}(t)|^2, d_{cal}^{s,r}(m, t) = R_{s,r} p \quad (34)$$

Lagrange functional with model parameter $m \equiv c$

$$L(m, p, \bar{p}) = C(m) + \langle \bar{p}, (\frac{1}{c^2} \partial_{tt} - \nabla^2) p - f \rangle_{\Omega \times [0, T]} \quad (35)$$

① forward wave equation:

$$\frac{\partial L}{\partial \bar{p}} = 0 \Rightarrow (\frac{1}{c^2} \partial_{tt} - \nabla^2) p = f \quad (36)$$

② adjoint state equation: different misfit C only change adjoint source

$$\frac{\partial L}{\partial p} = 0 \Rightarrow (\frac{1}{c^2} \partial_{tt} - \nabla^2) \bar{p} = -\frac{\partial C}{\partial p} = -R^\dagger (Rp - d_{obs}) \quad (37)$$

③ update the model based on the gradient

$$\frac{\partial L}{\partial m} = 0 \Rightarrow \nabla_m C = -\frac{2}{c^3} \int_0^T dt \bar{p} \partial_{tt} p \quad (38)$$

1. Forward equation:

$$\begin{cases} \rho \partial_t \mathbf{v} = D\boldsymbol{\sigma} + \mathbf{f}_v \\ \partial_t \boldsymbol{\sigma} = CD^T \mathbf{v} - \textcolor{blue}{C} :: \Gamma \sum_{\ell=1}^L y_\ell \boldsymbol{\xi}_\ell + \mathbf{f}_\sigma \\ \partial_t \boldsymbol{\xi}_\ell + \omega_\ell \boldsymbol{\xi}_\ell = \omega_\ell D^T \mathbf{v}, \quad \ell = 1, \dots, L, \end{cases} \quad (39)$$

2. Adjoint equation:

$$\begin{cases} \rho \partial_t \bar{\mathbf{v}} = D\bar{\boldsymbol{\sigma}} + \sum_{\ell=1}^L \textcolor{blue}{D}\bar{\boldsymbol{\xi}}_\ell + \Delta d_v \\ \partial_t \bar{\boldsymbol{\sigma}} = CD^T \bar{\mathbf{v}} + C\Delta d_\sigma \\ \partial_t \bar{\boldsymbol{\xi}}_\ell - \omega_\ell \bar{\boldsymbol{\xi}}_\ell = \omega_\ell y_\ell (\textcolor{blue}{C} :: \Gamma) C^{-1} \bar{\boldsymbol{\sigma}}, \quad \ell = 1, \dots, L. \end{cases} \quad (40)$$

where

$$\Gamma = \begin{bmatrix} Q_{11}^{-1} & Q_{12}^{-1} & Q_{13}^{-1} & Q_{14}^{-1} & Q_{15}^{-1} & Q_{16}^{-1} \\ Q_{21}^{-1} & Q_{22}^{-1} & Q_{23}^{-1} & Q_{24}^{-1} & Q_{25}^{-1} & Q_{26}^{-1} \\ Q_{31}^{-1} & Q_{32}^{-1} & Q_{33}^{-1} & Q_{34}^{-1} & Q_{35}^{-1} & Q_{36}^{-1} \\ Q_{41}^{-1} & Q_{42}^{-1} & Q_{43}^{-1} & Q_{44}^{-1} & Q_{45}^{-1} & Q_{46}^{-1} \\ Q_{51}^{-1} & Q_{52}^{-1} & Q_{53}^{-1} & Q_{54}^{-1} & Q_{55}^{-1} & Q_{56}^{-1} \\ Q_{61}^{-1} & Q_{62}^{-1} & Q_{63}^{-1} & Q_{64}^{-1} & Q_{65}^{-1} & Q_{66}^{-1} \end{bmatrix} \quad (41)$$

3. Gradient expression (Yang et al., 2016a):

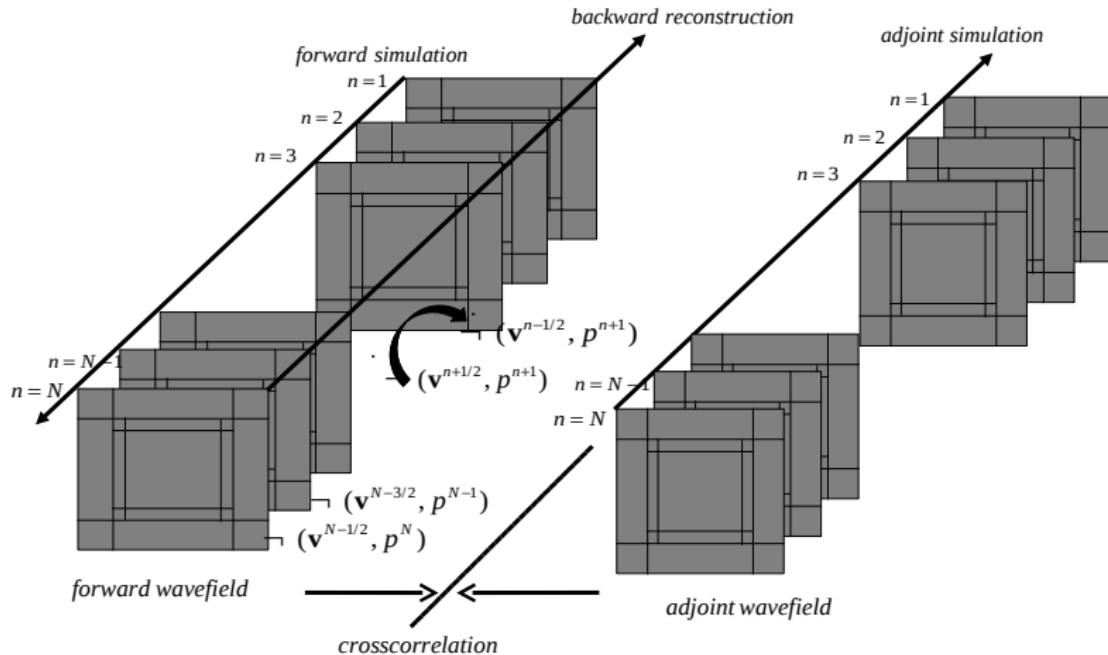
$$\begin{aligned}\frac{\partial \chi}{\partial \rho} &= - \int_0^T dt \bar{\mathbf{v}}^\dagger \partial_t \mathbf{v}, \\ \frac{\partial \chi}{\partial C_{IJ}} &= \int_0^T dt \bar{\boldsymbol{\sigma}}^\dagger C^{-1} \frac{\partial C}{\partial C_{IJ}} C^{-1} (\partial_t \boldsymbol{\sigma} - \mathbf{f}_\sigma), \\ \frac{\partial \chi}{\partial Q_{IJ}^{-1}} &= \int_0^T dt \bar{\boldsymbol{\sigma}}^\dagger C^{-1} (C \ddot{\colon} \frac{\partial \Gamma}{\partial Q_{IJ}^{-1}}) \left(\sum_{\ell=1}^L y_\ell \boldsymbol{\xi}_\ell \right), \quad \frac{\partial \chi}{\partial Q_{IJ}} = -Q_{IJ}^{-2} \frac{\partial \chi}{\partial Q_{IJ}^{-1}}.\end{aligned}\quad (42)$$

4. Constant-Q approximation by Least-squares method (Blanch et al., 1995; Yang et al., 2016a)

$$\min_{\gamma_\ell} \chi_1^Q, \quad \chi_1^Q = \int_{\omega_{\min}}^{\omega_{\max}} \left(\sum_{\ell=1}^L \gamma_\ell \frac{\omega_\ell \omega}{\omega^2 + \omega_\ell^2} - \gamma^{-1} \right)^2 d\omega. \quad (43)$$

in which

$$Y_\ell^{IJ}(\mathbf{x}) = y_\ell Q_{IJ}^{-1}(\mathbf{x}) \text{ with } y_\ell = \gamma \gamma_\ell. \quad (44)$$



It is mandatory to access incident wavefield backwards to build FWI gradient (or apply imaging condition in RTM)

- ① reading the **stored forward wavefield** from the disk, even with data compression (Sun and Fu, 2013; Boehm et al., 2015)
Reading disk memory is extremely slow for I/O intensive problems!
- ② inferring from the final snapshots and the saved boundaries via **reverse propagation (RP)** (Tromp et al., 2005; Dussaud et al., 2008; Clapp, 2008; Yang et al., 2014):
Efficient: Computation is much faster compared with disk accessing; may involve large 3D boundary storage, which can be significantly reduced using interpolation (Yang et al., 2016c);
- ③ remodeling using **checkpointing** (Griewank, 1992; Griewank and Walther, 2000; Symes, 2007; Anderson et al., 2012) from stored state to another state: Much better than disk reading, more expensive compared with reverse propagation due to repeated modeling!
- ④ checkpointing-assisted reverse-forward simulation (**CARFS**) =RP+checkpointing (Yang et al., 2016b) works in both attenuating and non-attenuating medium!

Reverse propagation based on the final snapshot and stored boundaries:

- forward modeling:

$$p^{n+1} = 2p^n - p^{n-1} + \Delta t^2 v^2 \nabla^2 p^n \quad (45)$$

store boundary at each forward timestepping

- reverse propagation:

$$p^{n-1} = 2p^n - p^{n+1} + \Delta t^2 v^2 \nabla^2 p^n \quad (46)$$

inject boundary at each backward timestepping

- Goal:
 - ① understand the fundamental gadgets in Madagascar
 - ② write codes within the framework of Madagascar
 - ③ reproduce numerical experiments using SConstruct
- Method: FDM
- Steps:
 - ① forward modeling with Clayton-Enquist ABC
 - ② wavefield reconstruction by RP+stored boundaries
 - ③ full waveform inversion
- Where is the exercise?
 - ① RSFSRC/book/xjtu/modeling2fwi
 - ② <https://yangpl.wordpress.com/activities/>

- Seiscope consortium for financial support on the travel
- Community effort for developing Madagascar: a great tool
- Sergy Fomel for the invitation
- ETH Zurich for providing the sharing opportunity

Thanks for your attention!

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